Development of Multi-axle Semitrailers in Ontario

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Ontario in North America

Ontario

Canada

United States

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Trucking in Ontario

- 38% of Canada's population live in Ontario
- 50% of truck trips in Canada travel in Ontario
 - One third of large trucks are from another jurisdiction
- 3.5 million trucks cross the Ontario US border per year, or one every 9 seconds



Advent of Multi-axle Semitrailers



Ontario Bridge Formula, 1970

Reflected the actual capacity of bridges Became the axle and gross weight regulation Increased weight from 33,000 to 63,500 kg Intended to make Ontario more competitive No restrictions on Configuration Number, type or location of axles



What was Expected



What Emerged









Lots of liftable axles !



Metrication, 1978

- The bridge formula was quickly found too complicated to enforce
- A legislated tolerance was added to allowable axle weights
- New tables for allowable gross weight rounded bridge formula values up
- Weights increased 5-8%
- No configuration controls, though the tables implicitly encouraged B-trains over A-trains

Technology

48 ft Semitrailers, 1984

- Adopted by US in 1982
 - Ontario matched this in 1984, to allow free movement of tandem semitrailers across the border
- The extra length allowed one more axle on a semitrailer



More New Configurations

For Ontario



For Ontario into Michigan



National Harmonization



National Initiative

- Diverse increases in weight by provinces
- Provincial Committee on Vehicle Weights and Dimensions formed, 1975
- Bridge studies led to road and bridge improvements, 1975-85
- CCMTA/RTAC Vehicle Weights and Dimensions Study, 1984-86
- National Memorandum of Understanding on Vehicle Weights and Dimensions, 1988

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Ontario Response, 1989

- Public pressure prevented increases in semitrailer and double trailer length
- Industry pressure prevented phase out of liftable axles
- M.o.U. configurations were accommodated at existing lengths
- Ontario became a barrier



53 ft Semitrailers

- Standard in the US by the early 1990's
- More pressure on Ontario
- Adopted in 1994, with 25 m (82 ft) doubles
- Detailed configuration specifications per the M.o.U.

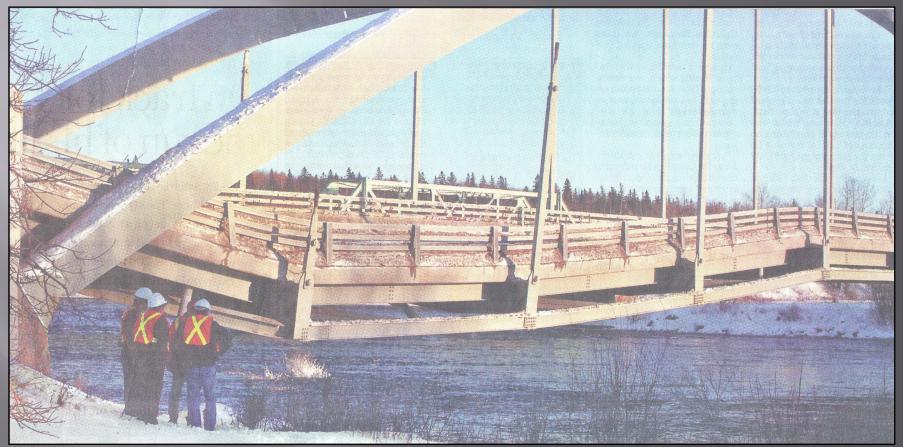


Eastern Provinces Harmonization

- Agreed to eliminate liftable axles, 1995
- Scuttled by industry in Ontario
 - Other five provinces proceeded
- Led to infrastructure and freight studies
- Interpretation of the infrastructure study showed trucks with liftable axles were costing Ontario \$300 million (Cdn) per year in highway maintenance and rehabilitation

Technology

Increasing Rate of Bridge Failure





Reform of Weights and Dimensions





Regulation of legal trucks
 Pilot programs introduced
 Permits introduced for operation of special truck configurations



Reform for Legal Vehicles

Phase 1, effective 1 January 2001

- Defined "Safe, Productive and Infrastructurefriendly" (SPIF) trailers
- Introduced self-steer tri-axle and self-steer quad
- Reduced the allowable gross weight of tri-axle semitrailers from 2006
- Phase 2, effective 1 July 2002
 - Required dump semitrailers built after 2002 to meet SPIF standards



SPIF - Safe Productive Infrastructure-Friendly



Self-steer tri-axle



Self-steer quad



Reform for Legal Vehicles

- Phase 3, 2006
 - Other multi-axle semitrailers with liftable axles
 - Doubles
- Phase 4, 2011
 - Straight trucks
 - Truck-trailer combinations
 - Everything else



Phase 3 Scope

Assessment by computer simulation of the dynamic performance of:

 Existing multi-axle semitrailers
 Candidate SPIF multi-axle semitrailers

 Test two 5-axle semitrailer configurations
 Doubles already addressed by M.o.U.



Ontario Configurations for Operation in Ontario

12S131 (48% of existing trailers)





Ontario Configurations for Operation into Michigan





Michigan Configurations that Operate into Ontario





Simulation Methodology

- Yaw/roll program
 - Compute responses to a standardized input
 - Compute performance measures
 - Compare these to performance standards
- Performance measures
 - Static roll threshold, high-speed offtracking
 - Load transfer ratio, transient offtracking
 - Low-speed offtracking, rear outswing, friction demand, lateral friction utilization, maximum self-steer angle

Dynamic Performance of Existing Configurations

Config	Lift Axles	SRT (g)	HSOT (m)	LTR	TOT (m)	LSOT (m)	RO (m)	FD
		>0.4	<0.46	<0.6	<0.8	<5.6	<0.2	<0.1
12S113	Down	0.39	0.53	0.60	0.81	4.00	0.10	0.68
12S113	Up	0.36	0.64	0.57	0.76	5.16	0.03	0.14
12S131	Down	0.39	0.56	0.58	0.79	4.00	0.09	0.61
12S131	Up	0.33	0.61	0.70	0.91	4.18	0.25	0.11
12S114	Down	0.43	0.48	0.59	0.78			High
12S114	Up	0.38	0.57	0.54	0.69	4.98	0.06	0.07
12S141	Down	0.43	0.51	0.61	0.86			High
12S141	Up	0.37	0.55	0.67	0.86	4.06	0.24	0.10

Candidate Configurations

Based on existing trailer configurations A self-steer axle replaced a rigid liftable axle Axle weights were equalized Axle spacings and spreads were adjusted to: Satisfy the bridge formula Balance the vehicle Retain current gross weight Self-steer axles with: Low, medium, or high centring force, or locked Single or dual tires

Candidate Configurations

Configurations for operation in Ontario **12S131** 12S113 **1**3S13 Configurations for operation into Michigan **12**S141 **12**S114



Dynamic Performance of Candidate Configurations

Config	SRT (g)	HSOT (m)	LTR	TOT (m)		RO (m)		LFU	MSS (deg)
	>0.4	<0.46	<0.6	<0.8	<5.6	<0.2	<0.1	<0.8	<20
125113	0.43	0.54	0.54	0.72	5.07	0.04	0.23	0.58	19.6
12S131	0.43	0.53	0.57	0.75	3.98	0.17	0.22	0.54	17.6
12S114	0.43	0.47	0.54	0.68	5.02	0.04	0.24	0.54	22.5
12S141	0.42	0.49	0.59	0.77	3.44	0.31	0.29	0.53	19.8
13513	0.41	0.49	0.52	0.64	5.15	0.04	0.12	0.79	17.1



Preferred Configuration for 12S113 and 12S114

- Self-steer axles:
 - Need low centring force
 - As close as possible to each other
 - As close as possible to the fixed axles
 - Need at least 25 deg of steer
 - Do not need to be locked at high speed



Preferred Configuration for 12S131 and 12S141

- Fixed axles moved rearward between selfsteer axles
- Self-steer axles need:
 - Low centring force
 - At least 25 deg of steer

Rear self-steer axle should be locked at high speed, and should lock and unlock automatically with speed



Issues for Test Program

- Validity of the warrant for the friction demand performance measure?
- Actual high-speed offtracking?
- Self-steer capability?
- Need to lock self-steer axles at high speed?
- Can self-steer axles introduce hazards not found on existing trucks?

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Can we trust the computer simulation?

Configuration 12S113



5,452 kg 18,125 kg 15,176 kg 22,900 kg

Gross weight 61,653 kg
Single tires on self-steer axles
28 deg self-steer



Configuration 12S131



5,447 kg 17,998 kg 7,692 kg 22,666 kg 7,692 kg

Gross weight 61,494 kg

Dual tires on self-steer axles

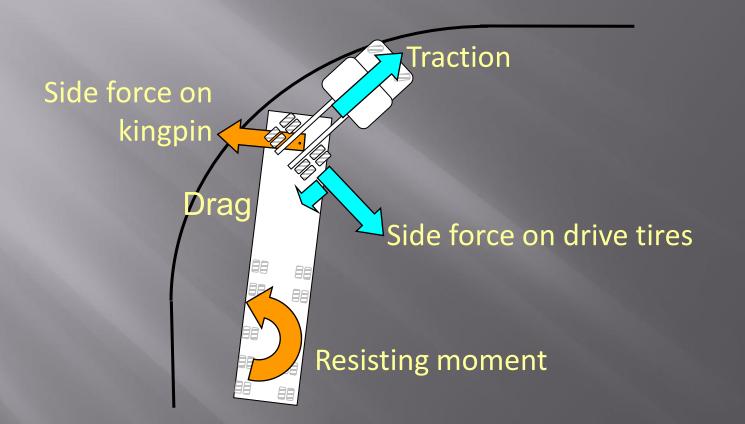
Nominal 20 deg self-steer, actually 18 degree

Test Program

- Low-speed turns on a low-friction surface
- Low-speed turns on real streets
- 0.2 g turn on 30.5 m radius
- 0.2 g high-speed turn
- SAE J2179 lane changes
- SAE J2179 lane changes at twice amplitude
- Provoked steer inputs to self-steer axles



Friction Demand



Friction demand = <u>Side force on drive tires</u> Vertical load on drive tires



Friction Demand

- High friction demand might lead to a jackknife in a low-speed turn
- Performance standard was set at 0.1
- Previous tests could not provoke a jackknife
- Tridems operate at 0.12 to 0.20, self-steer quads up to 0.25
- These trucks do not seem to jackknife
- Candidate trucks had higher friction demand

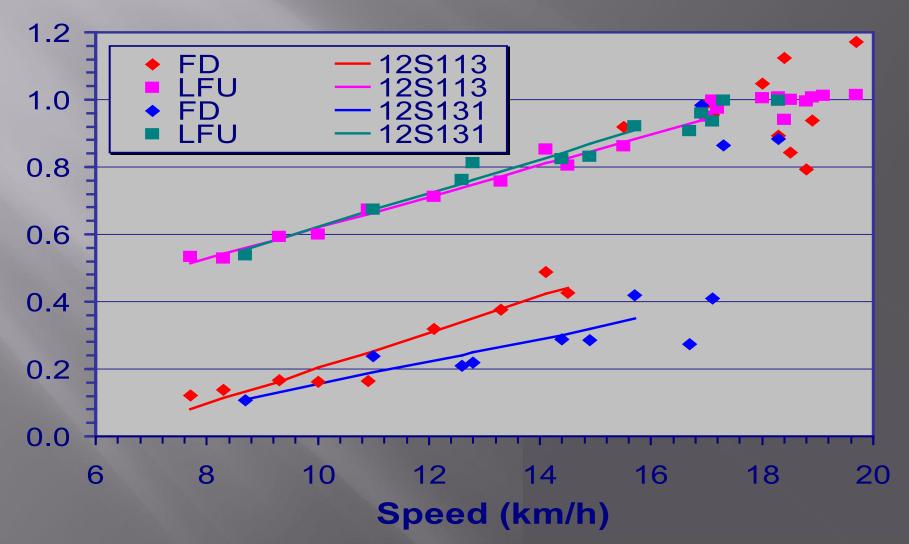
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Friction Demand Test

- Low-speed turns on a low-friction surface
- Friction demand set by adjusting the centring force or locking the self-steer axles
- Driver, data, and simulations all agreed that low self-steer axle centring force was best
- Both configurations jackknifed or ploughed out, but at speeds far higher than any driver would consider for a turn in such a truck

Technology

Friction Demand and LFU from Simulations of Test Runs



Friction Demand

- Friction demand depends on the self-steer axle settings, turn radius, and speed
 Carriers adjust self-steer axles for low friction demand to reduce tire wear
- Drivers choose a turn radius and speed that allows an easy (low friction demand) turn
- The friction demand performance measure did not appear strongly related to safety

Technology

Self-steer Capability

- Drove around interior roads at test site
- Configuration 12S113 had 28 deg of selfsteer
 - Plenty
- Configuration 12S131 had only 18 deg of self-steer
 - Marginal
 - More would reduce the risk of bottoming



Actual High-speed Offtracking

Warrant for performance standard is a curb strike, possibly causing a tripped rollover Performance standard of 0.46m leaves 0.08 m clearance for a vehicle is centred in its lane ▶ Test in 0.2 g turns showed: Inward offtracking at 27.5 km/h in a 30 m radius Outward offtracking at 80 km/h in a 250 m radius High-speed offtracking was typical for selfsteer quads

Actual High-speed Offtracking

~ 85 km/h in 192 m radius with 7.5 deg superevelation ~ 0.16 g unbalanced lateral acceleration



Actual High-speed Offtracking

- No outward offtracking at speeds typical on urban roads, which have curbs
- High-speed offtracking appears critical on roads with a speed limit of 80 km/h, which typically do not have curbs
- It is not significant on freeways, which have a design speed of 120 km/h or more



The Need to Lock Self-steer Axles at High Speed Lock allowed about 1 deg of free play Locking both self-steer axles of 113 trailer, or front axle of 131 trailer, had no evident effect Locking rear self-steer axle of 131 trailer moderated both high-speed and transient offtracking

A tight lock would be more effective



Potential Hazards of Self-steer Axles

Braked wheels on one side of self-steer axles to provoke self-steer, then ran off road Ran one wheel over speed bump Experienced lock-up and hard-over of both self-steering axles of 113 trailer during test No problem for driver to maintain control A 2S/1M ABS mitigates this risk Shimmy, if kingpin inclination not controlled

Technology

The Fidelity of the Computer Simulation

- Measured steer angle and speed from test fed as inputs into simulation
- Simulation responses reflected:
 - Both gross and small steer inputs seen in test
 - Changes in test vehicle parameters
 - Differences between test vehicles



Implementation

- All candidate configurations were defined in regulation, effective 1 January 2006
 - Self-steer angle based on offset from fixed axles
 - ABS on all axles
 - Split braking system
- Weight reductions for non-SPIF semitrailers built after 2005

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Weight reductions for all non-SPIF semitrailers from 2016

Thank you for your attention!



